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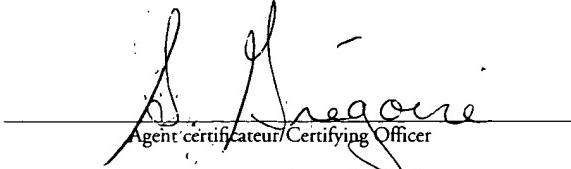
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Specification and Drawings, as originally filed, with Application for Patent Serial No:  
2,328,578, on December 15, 2000, by SHAW INDUSTRIES LTD., assignee of Amarjit  
Tathgur, Dilip K. Tailor and David Seepersaud, for "Method for Inductively Heating a  
Substrate and a Coating on Said Substrate".

  
Agent certificateur/Certifying Officer

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O P I C  C I P O

ABSTRACT

A method of heating a substrate and a coating on the substrate. A suscepter element is applied on the coating and the element and the substrate are inductively energized  
5 to cause the substrate and the coating to be heated.

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The present invention relates to a method for inductively heating a substrate and a coating on the substrate, and provides a method comprising applying on the coating a susceptor element, wherein the susceptor element and substrate are inductively heatable, and inductively energizing the element and the substrate to cause the substrate and coating to be heated.

The present method overcomes problems that can arise when attempting to heat substrates having coatings,

10 particularly relatively thick and poorly heat conductive, for example plastics coatings. For example, while it is known to employ induction heating to heat polyolefin coated pipe, difficulties can arise when the coating is relatively thick. For example, in the case of applying a covering to

15 a weld joint in polypropylene coated pipe, with certain covering systems, it is desired to raise the temperature of the metal at the cutback portion to a minimum of 165°C, preferably about 180°C and the exterior of the polypropylene covering to a minimum of about 145°C, but

20 more preferably about 165°C. Where the coating is greater than about 3 mm thick, for example 6.0 mm thick or greater, it has been found that induction heating is incapable of raising the exterior surface of the polypropylene coating to the desired temperature without prolonged and intensive

25 induction heating that tends to excessively heat the steel substrate with the result that the coating components degrade, deform and decompose.

With the arrangement of the invention, wherein the coating is heated from the outside through an inductively heated susceptor element, as well as from the inside through the inductively heated substrate, it has surprisingly been found that it is possible to heat the coating to a desired temperature without encountering the problems of deformation, degradation and decomposition

35 referred to above.

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Advantageously, the susceptor element may function as a mould as described in more detail in our copending U.S. patent application serial No. 09/684,788 filed October 10, 2000, the disclosures of which are incorporated herein by reference.

The procedure of the present invention has a number of other surprising advantages. It has been found that the procedure of the invention provides the opportunity to tailor the temperature profile of the substrate and of the coating to meet the requirements of, for example, a particular covering system as may be dictated by, for example, pipe diameter, wall thickness, coating type and coating thickness.

The inductive frequency may be such as to effect skin effect heating or may heat the substrate and susceptor element through their thickness.

The invention will be described in more detail, by way of example only with reference to the accompanying drawings.

Fig. 1 is a partially schematic longitudinal cross section through a wall of a coated pipe joint in the course of application of a heat shrinkable covering.

Fig. 2 is a partial cross section through a coated pipe wall showing heating of a discrete area of the wall for the purpose of application of a repair patch.

Fig. 3 shows the completed repair.

With reference to the accompanying drawings. Fig. 1 shows pipe sections 11 and 12 welded together at a weld joint 13. Outwardly from the joint 13, each pipe section 30 11 and 12 has a mainline coating 14 and 16 thereon. The main line coating may comprise a polyolefin, for example

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polypropylene. The pipes 11 and 12 are usually steel. End portions 19 and 21 of the pipe are bare of the coatings 14 and 16 to allow the weld to be accomplished, and are usually referred to as cut-back portions. These cut-back 5 portions 19 and 21 may have a coating of a curable primer composition, for example an epoxy composition. The coatings 14 and 16 may be, for example, of a multi-component type, comprising an outer polyolefin, for example polypropylene, coating on an inner polypropylene adhesive 10 coating, the latter being applied directly on the metal pipe, or over the above-mentioned curable primer.

For the purpose of applying a heat shrink sleeve over the joint area, it is desired to heat the coatings 14 and 16 in the regions that will be overlapped by the sleeve and 15 slightly outwardly beyond the edges of the sleeve to a temperature in excess of the activation temperature for the sleeve, for example as described in our above mentioned U.S. patent application serial No. 09/684,788.

Over these regions, a susceptor element that, in the 20 example shown, is in the form of a metal band is placed. The metal band may be, for example, a flexible metal strip that extends around the girth of the pipe, and has its ends overlapping and connected by quick release fasteners, such as toggle latches or the like. Preferably, the metal 25 bands, when secured around the girth of the pipe snugly engage the outer surface of the coatings 14 and 16.

In the example shown in the drawings, a heat insulating band is applied over the exterior of the metal band 22, to reduce heat loss.

30 Outwardly from the assembly is shown the induction coil 24.

In use, the induction coil is energized in order to inductively heat the metal of the pipes 11 and 12 as well

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as the weld joint 13, and to heat the metal bands 22, so that the coatings 14 and 16 are heated by conduction from the bands 22 as well as from the metal of the pipes 11 and 12.

5        When the bare portions 19 and 21 and the coatings 14 and 16 have achieved desired temperatures, the induction coil is slid to one side, the susceptor elements 22 and insulation bands 23 removed and a heat activatable sleeve applied over the pipe joint area as described in our above  
10 mentioned U.S. patent application serial No. 09/684,788.

It may be noted that, during the heating operation, the metal bands 22 perform the function of moulds, serving to maintain the uniformity, continuity and profile of the coatings 14 and 16.

15       It is contemplated that susceptor elements in the form of structures other than bands can be employed.

For example, referring to Fig. 2, this illustrates application of a susceptor element 26 in the course of repair of a puncture or holiday 27 in a coating 28 on a  
20 pipe wall 29. The susceptor element may be adapted for heating a discrete area and will therefore be substantially smaller in size than the girth of the pipe, but should be somewhat greater than the size of the puncture. For example, in the case in which the puncture 27 is  
25 approximately 25 mm x 25 mm, the susceptor element 26 may be, for example, a metal plate approximately 50 mm x 50 mm. Desirably, the susceptor element 26 has a curvature matching the curvature matching the curvature of the pipe wall 29 in use, for example, a 50 mm x 50 mm metal plate  
30 with the curvature of the pipe wall 29 is placed over the puncture 27 and the element 26, together with the underlying portion of the pipe wall 29 is subjected to an induction field applied from an inductive coil 31, thereby heating the coating 28. Once the coating 28 has been

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heated to a desired temperature, a repair patch comprising, for example, a polypropylene backing piece 32, as seen in Fig. 3 and having an adhesive coating on its underside is applied over the heated coating 24 and may be further  
 5 heated, for example by application of hot gas, for example from a torch flame, or by pressing the repair patch with the heating plate 26 and subjecting it to the induction field, so that the adhesive has cause to melt and flow to fill the opening 27, as seen in Fig. 3. The assembly is  
 10 then allowed to cool.

In order to further illustrate the present invention, Comparative Examples and an Example will be given.

#### Comparative Examples

##### Comparative Example I

15 A pipe joint area between polypropylene coated pipe was heated by induction heating without use of a susceptor element.

The pipe joint had the following characteristics.

	<u>Pipe Diameter</u>	<u>600 mm</u>
20	Pipe wall thickness	37.5 mm
	Steel total cutback (length of portion bare of coating)	300 mm
25	Coating length to be heated from the edge of cutback	75 mm
	Coating thickness	2.5 mm

The pipe joint area was heated using an induction coil, and the temperature of the coatings and the steel were determined using thermocouples.

30 The induction heating was applied until the coating

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surface, heated by conduction from the underlying substrate, attained a temperature of 160°C. At this point, the steel had attained a temperature of 200°C. There was some blistering and delamination of the coating, and this  
5 was prevented by use of a silicon rubber mould band wrapped around the coating as described in U.S. serial No. 09/684,788.

Comparative Example II

Comparative Example I was repeated except the  
10 thickness of the coating was 6.0 mm.

When the steel had attained a temperature of 200°C, the coating surface had reached only 90°C, and this was attributed to difficulties in heat transfer through the thick coating.

15 When the steel temperature was raised to 215°C, the coating surface attained 100°C. In subsequent experiments, the steel temperature was raised to as high as 250°C, and the coating temperature was raised to about 130°C, but at this point a lot of smoke was observed, the fumes being  
20 emitted from the coating. The coating outside the mould area started to blister, and the epoxy primer on the steel cutback started to degrade and emit fumes. It became clear that the required coating surface temperature could not be attained by relying on heat transfer from the metal  
25 underneath.

Example

The procedure of Comparative Example II was repeated. However, before commencing induction heating, a 1.5 mm thick, 90 mm wide steel band was applied on the coating on  
30 each side of the cutback. Using a 400 Hz frequency on the induction coil, the steel was heated to 200°C, and the temperature of the coating under the steel band was

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measured using a thermocouple wire embedded in the coating at 2.0 mm depth. The coating temperature of 155°C was measured. After the heating was completed, a polypropylene shrink sleeve was applied. It was found that during the  
5 shrinking of the sleeve with a propane torch, the coating temperature rose to 168°C. Subsequent test of the cooled sleeve showed excellent adhesion of the sleeve to the coating, as well as to the steel.

More generally, an advantage of the method of the  
10 present invention is that it permits the user to manipulate and tailor the temperature profile of a weld joint and more specifically, the temperature achieved at the metal surface of the cutback and in the coating, respectively, and can accommodate variations in the characteristics of the  
15 pipeline structure, differing, for example, with respect to the pipe diameter, wall thickness, coating type and the coating thickness.

If has been found that such manipulation can be achieved by selection of various characteristics of the  
20 induction heating procedure and, more specifically of the susceptor elements. These include the following.

#### 1. Resistivity of the Susceptor Element

Materials such as steel with relatively higher resistivity will respond more readily to the induction  
25 field and heat up much faster, as opposed to materials such as aluminium with much lower resistivity. The steel used in the above described Example was stainless steel with a resistivity of 24. Using an open circuit on the band, the desired temperatures were achieved in 6 min. at 60 KW  
30 power. The temperature profile and the heating rate can therefore be tailored by selecting a band or other susceptor element with an appropriate resistivity. Usually the susceptor element will be of metal, but it is contemplated that conductive non-metals may be employed.

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2. Thickness of the Susceptor Element

The greater the thickness, the slower the temperature rise of the susceptor element. A desired differential between the rates of heating of the cutback area and of the 5 coating can, therefore, be tailored by selecting the thickness of the susceptor element.

3. Time to Heat

By adjusting the power of the induction coil, the rate of heating can be adjusted. It has been found that, when 10 heating is done at a slower rate, the final coating surface temperature is higher. This can be explained by the fact there is more time available for heat diffusion from the metal band (as well as from the pipe metal underneath) into the coating.

15 4. Insulation

A heat insulating material, such as calcium silicate or glass fibre may be placed under the susceptor element and can serve to slow down the heat transference, thereby allowing control of the temperature of the coating surface.

20 In the above Example, a Teflon coated glass fibre fabric was adhered to the bottom of the band. By using a fabric of different thickness, or of a different kind of texture, for example smooth versus rough texture, the temperature of the coating can be changed as desired. The 25 Teflon coated fabric provides the further advantage that it acts as a release agent, to prevent the steel band or other susceptor element from bonding to the coating.

Further, it has been found that, when the top of the susceptor element is exposed, the ambient air temperature 30 dissipates some of the heat from the susceptor element. This can result in a significant heat loss in sub-zero

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conditions. Such heat loss can be reduced or avoided by placing a layer of heat insulation on top of the susceptor element. For example, a 10.00 mm thick calcium silicate insulation layer may be applied over the susceptor element  
5 to prevent heat loss.

5. Perforate Susceptor Element

It has been found that by reducing the mass of the susceptor element, for example by employing a susceptor element that is perforate or foraminous, the heating rate  
10 can be slowed. Examples of perforate or foraminous materials that may be used include metal walls, such as steel wool, metal mesh, for example steel mesh fabrics such as netting, and perforate susceptor elements such as perforated steel bands.

15 6. Open or Closed Circuit

The Example described above was carried out keeping an open circuit in the heating band. This was achieved by disposing electrical insulation between the overlapping ends of the band. In the Example above, at 60 KW, heating  
20 of the coating to 155°C was achieved in 6 min. However, when a closed circuit was used, wherein the overlapped ends were in contact, the band heated up extremely fast. The 155°C temperature was achieved in 35 seconds. Hence, by using an open or a closed circuit, the heating rate can be  
25 altered significantly.

It may be noted that the use of the susceptor element in accordance with the invention is not limited to the application of heat shrink sleeves. Other joint protection systems such as flame sprayed powders, heat shrink tapes  
30 and welded wrap-around polypropylene sheets, for example polypropylene sheets can be applied to substrates heated employing the method in accordance with the invention.

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CLAIMS:

1. Method for heating a substrate and a coating on said substrate comprising applying on the coating a susceptor element, wherein said susceptor and substrate are inductively heatable, and inductively energizing the element and substrate to cause said substrate and coating to be heated.
2. Method as claimed in claim 1 wherein a heat insulation material is provided on an outer side of the susceptor element.
3. Method as claimed in claim 1 or 2 wherein a inner heat insulation material is interposed between the susceptor element and the coating.
4. Method as claimed in claim 5 wherein the inner insulation material includes a release layer.
5. Method as claimed in any preceding claim wherein the susceptor is perforate or foraminous.
6. Method as claimed in any preceding claim wherein the susceptor element provides an open circuit.
7. Method as claimed in any of claims 1 to 5 wherein the susceptor element provides a closed circuit.
8. Method of repairing an opening in a coating on a substrate comprising heating said coating employing a heating method as claimed in any of claims 1 to 7 to heat the coating before applying a patch.
9. Method as claimed in claim 8 comprising heating said coating to at least an activation temperature for said patch or for a coating on said patch.

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10. Method as claimed in claim 8 or 9 wherein the substrate is a tubular article and the susceptor element is curved to conform to a surface curvature of the article.

11. Method of applying a coating or covering to a weld joint between tubular substrates having mainline coatings comprising heating said substrates and coatings employing a heating method as claimed in any of claims 1 to 7 before applying said coating or covering.

12. Method as claimed in claim 11 wherein said covering comprises a heat shrink sleeve and said heating method comprises heating said mainline coatings adjacent the weld joint, and wherein said susceptor element comprises a pair of band form elements applied around the girth of the mainline coatings of the tubular article adjacent the weld joint.

13. Method as claimed in claim 12 including heating the coatings and the articles adjacent the weld joint to at least an activation temperature for the sleeve or for a coating on the sleeve.

14. Method as claimed in any preceding claim wherein the coating comprises polyolefin.

15. Method as claimed in claim 14 wherein the polyolefin is polypropylene.

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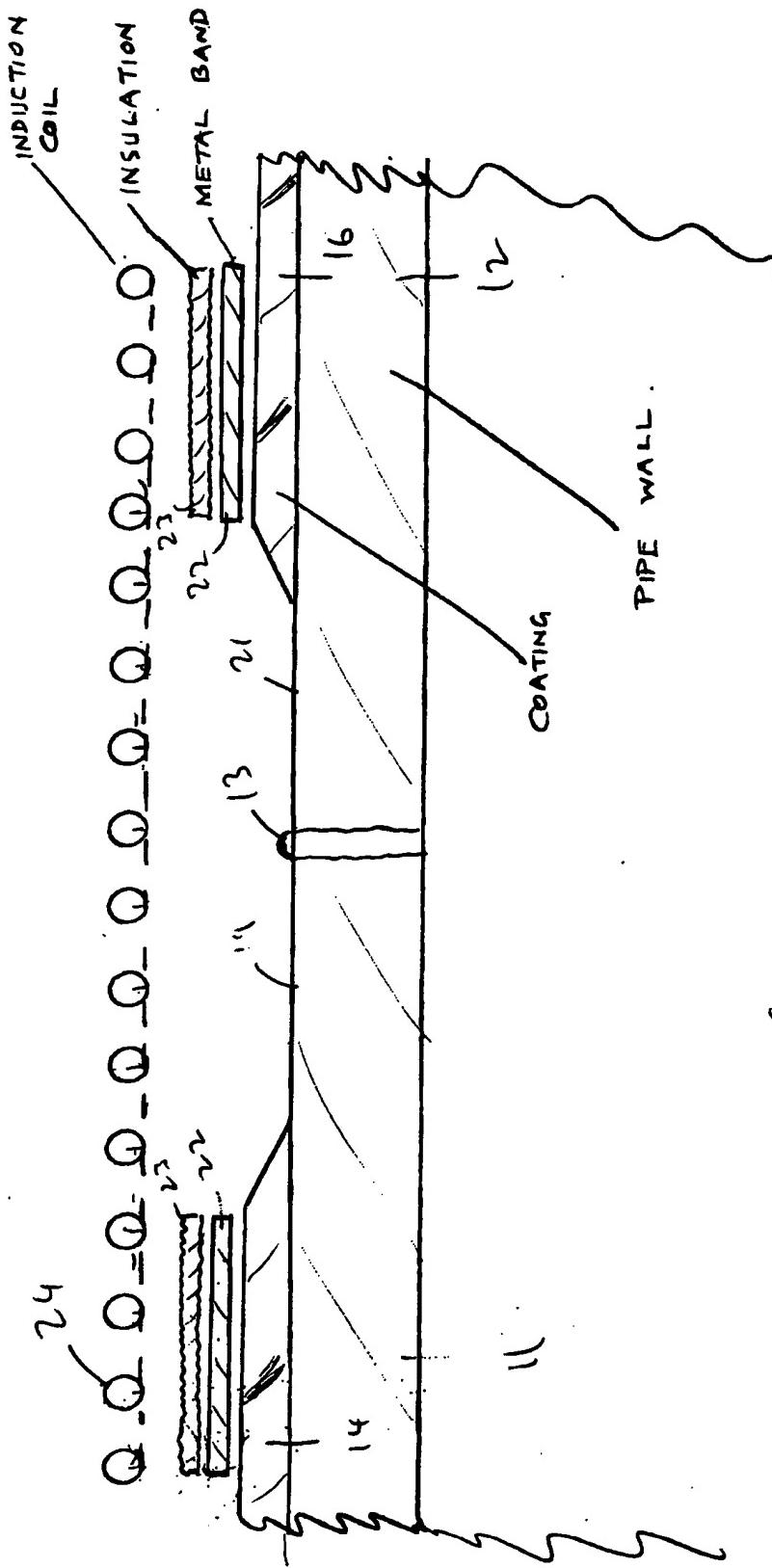
FIGURE 1  
INDUCTION HEATING USING STRESS BANDS

FIG. 1

**REPAIRS OF DISCRETE DAMAGED AREAS.**

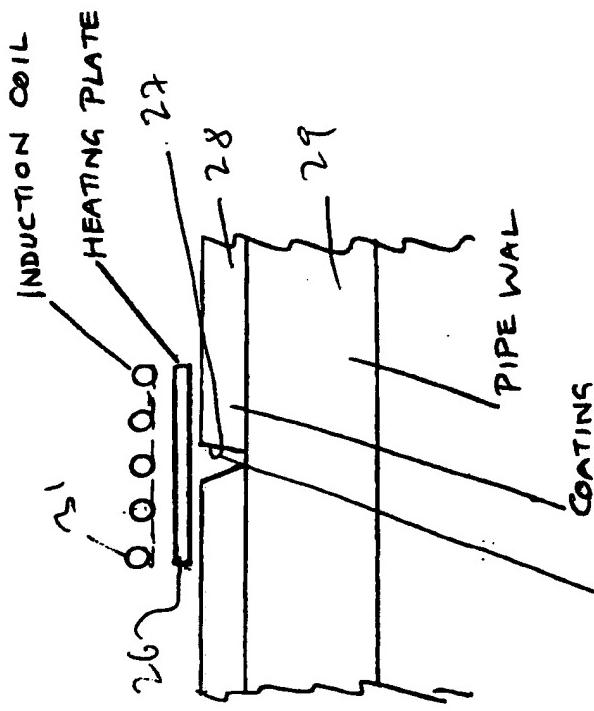
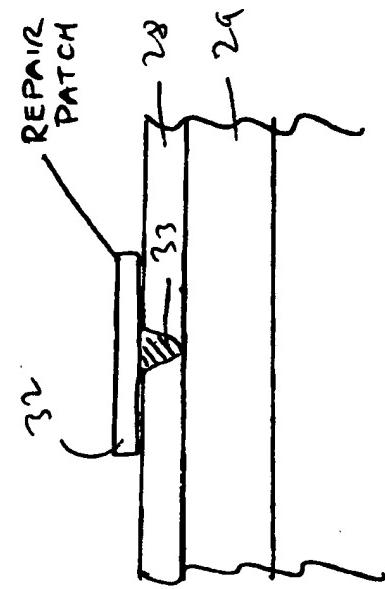


fig. 2

- 2 a) Heat the area around the damage with an induction heated plate



- fig. 3
- 2 b) Apply repair patch over the damage

fig. 3